



Numerical Simulation of Cascaded Arc for Ar and H₂ gases

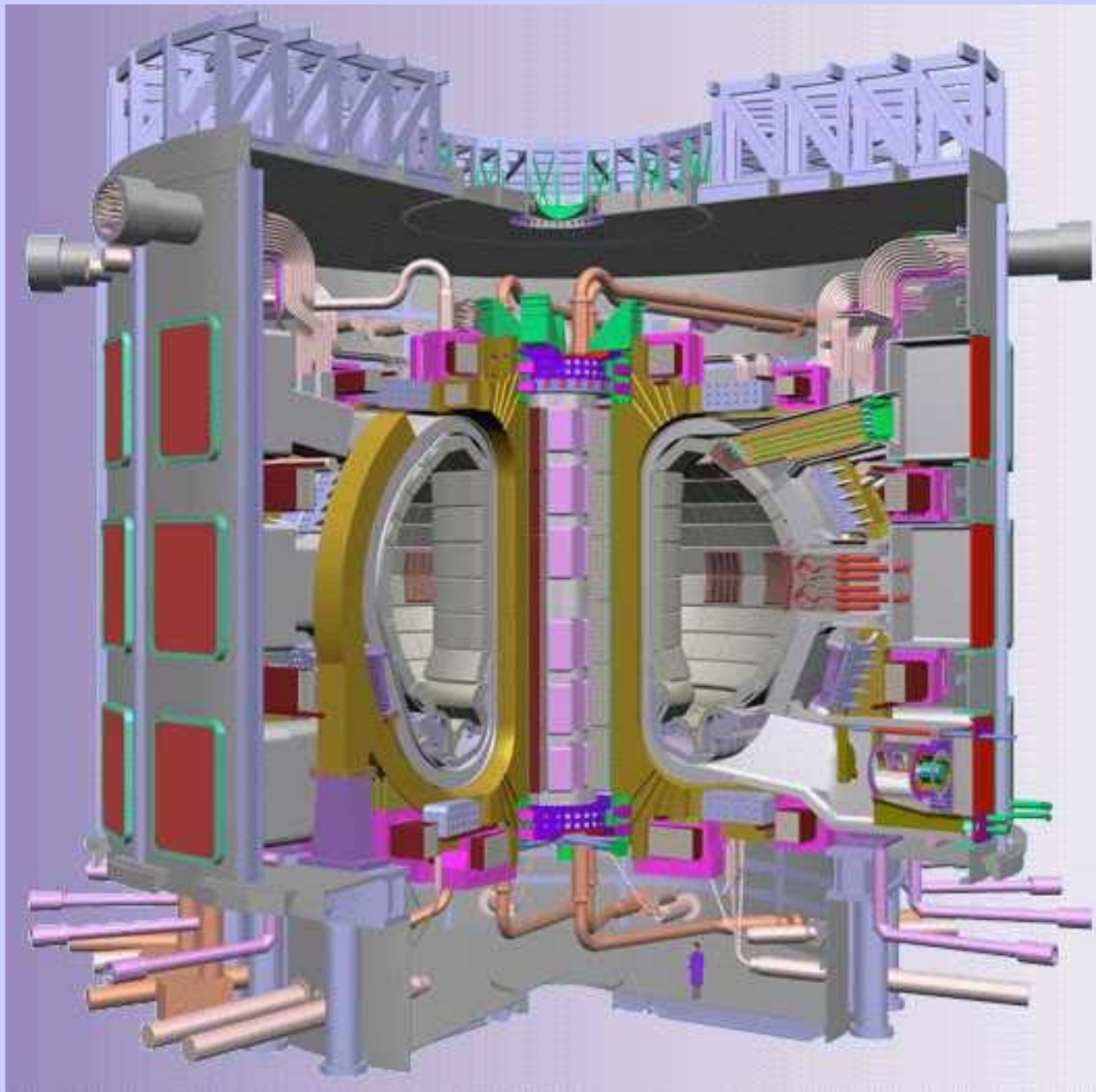
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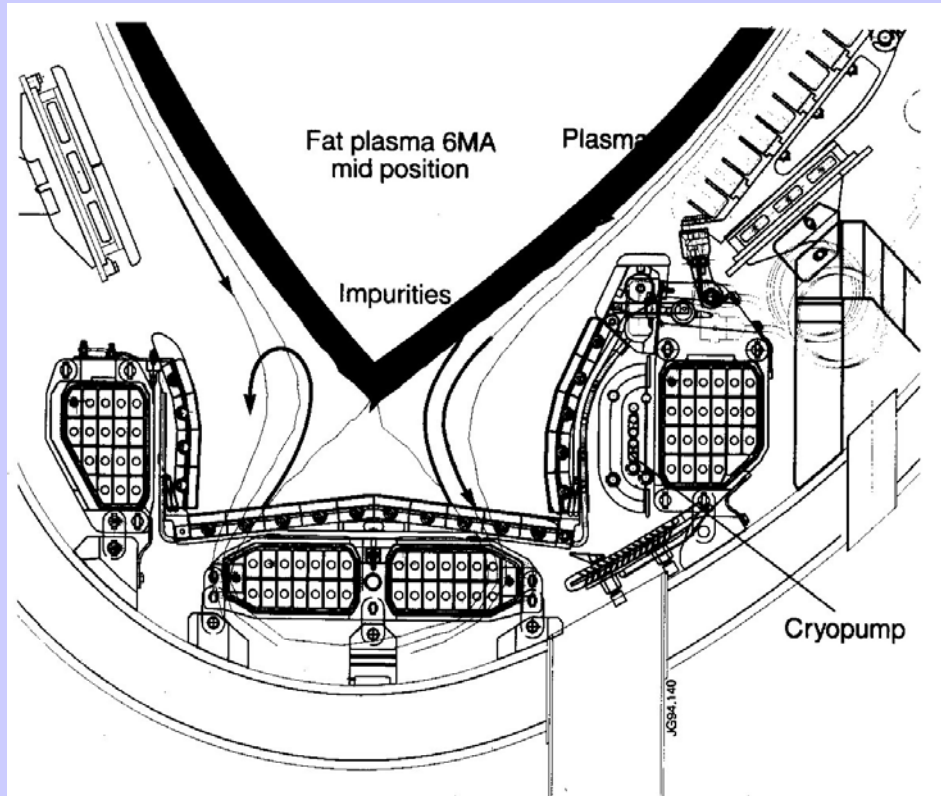
Introduction

- **Magnum-psi Project:** (MAGnetised plasma Generator and NUmerical Modelling for Plasma Surface Interaction studies)
- **Aim of Magnum-psi project:**
 - Study of plasmas expected in the divertor region of future Tokamak ITER
 - particle flux density $\sim 10^{22}$ - $10^{24} \text{ m}^{-2}\text{s}^{-1}$
 - electron and ion temperature $\sim 1 \text{ eV}$
 - magnetic field $\sim 5 \text{ T}$
 - Study of industrial applications of plasmas like deposition, etching etc.
- **Plasma Source:** Cascaded Arc
- **Tool:** PLASIMO (PLASma SIMulation MOdel).



ITER Diagram

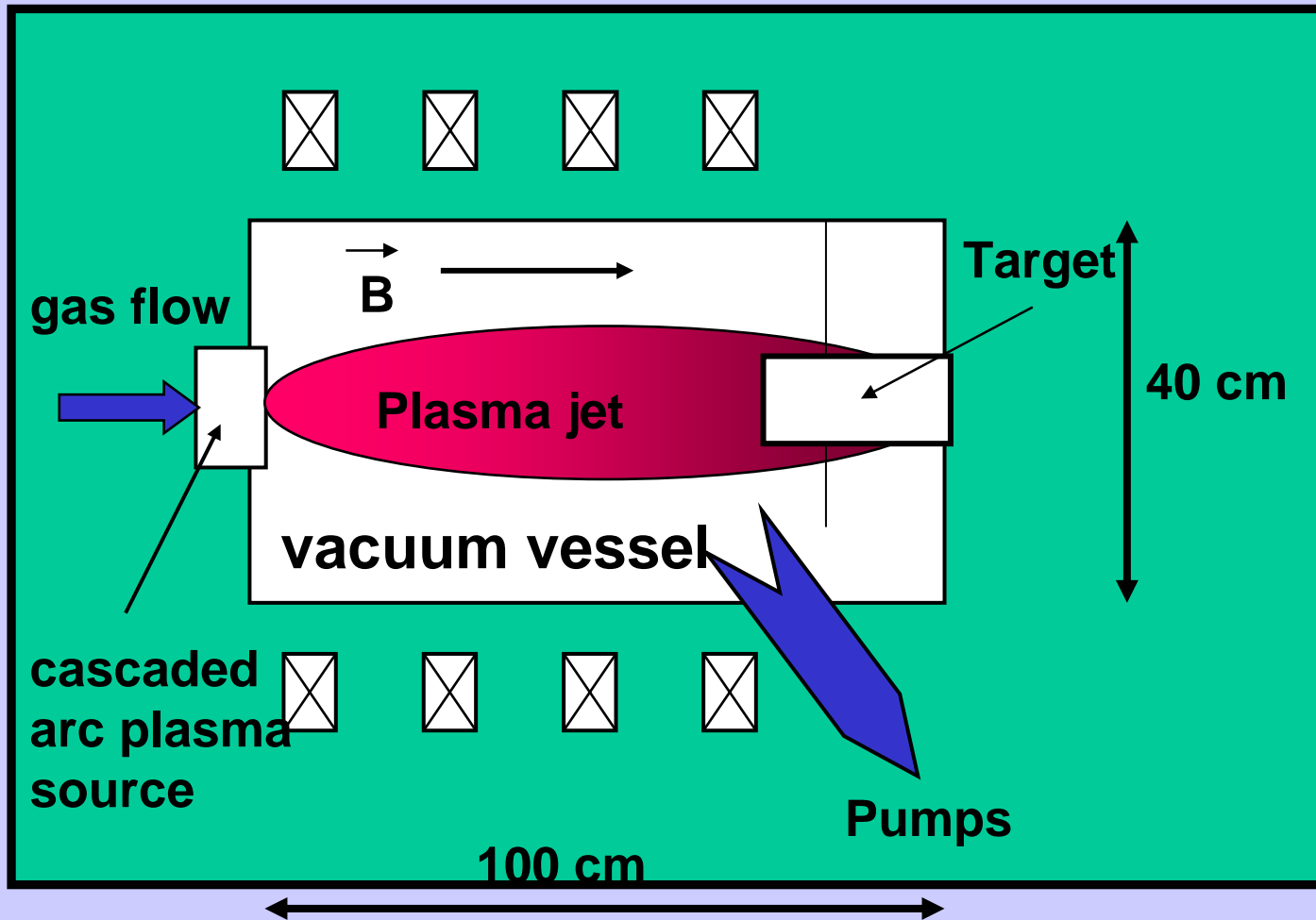
Divertor region of a Tokamak



Conditions at surface of ITER Divertor:

- particle flux density at surface $\sim 10^{24} \text{ m}^{-2}\text{s}^{-1}$
- electron and ion temperature $\sim 1 \text{ eV}$
- magnetic field $\sim 5 \text{ T}$

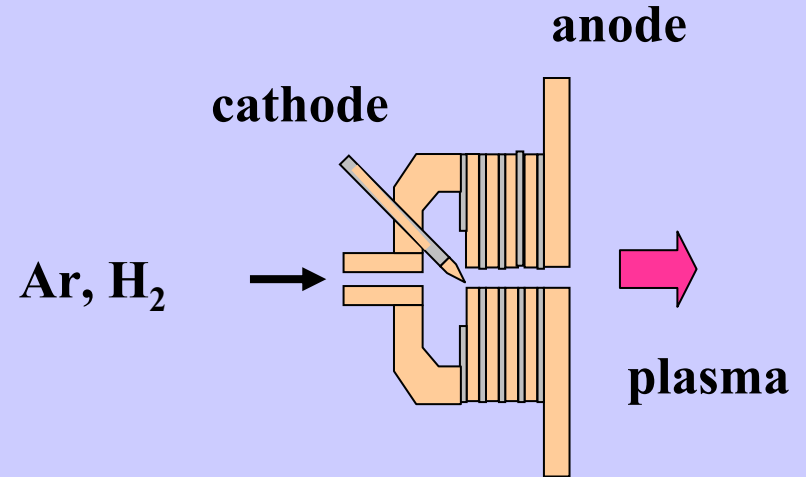
Pilot-psi experimental set-up



Plasma Source Geometry

Straight arc channel:

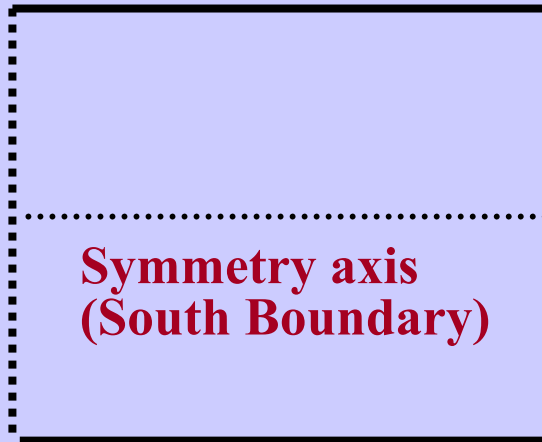
4 mm diameter, 32 mm length



**Channel Wall
(North Boundary)**

**Inlet
(West Boundary)**

H₂, Ar



**Outlet
(East Boundary)**



Plasma

Grid: 16 radial×64 axial points

Mathematical Model

With the use of a two-dimensional hydrodynamical model, plasma processes in the arc are simulated. The governing equations in the model are:

$$\text{Particle balance equations: } \vec{\nabla} \cdot \left(n_h \vec{u} \right) - \vec{\nabla} \cdot \left(D_h \vec{\nabla} n_h \right) = S_h$$

D_h and \vec{u} are the diffusion coefficient of species h and the plasma bulk velocity respectively, while S_h denotes the net production of species h due to the collisional-radiative processes

$$\text{Total Continuity equations: } \vec{\nabla} \cdot \left(\rho \vec{u} \right) = 0$$

$$\text{Momentum balance : } \vec{\nabla} \cdot (\rho \vec{u}_i \vec{u}) = - \left[\frac{\vec{\nabla} p}{i} \right] + \left[\frac{\vec{\nabla} \cdot \tau}{i} \right]$$

where i denotes the axial or radial component and τ viscous stress tensor.

$$\text{Energy balance heavy particles : } \vec{\nabla} \cdot \left(\rho_h \varepsilon_h \vec{u} \right) + p_h \vec{\nabla} \cdot \vec{u} + \vec{\nabla} \cdot \vec{q}_h = \tau_h \dot{\vec{\nabla}} \vec{u} + Q_h$$

where ε_h is the internal energy per unit mass of the heavy particle. The heat flux is $\vec{q}_h = -\kappa \vec{\nabla} T$ and Q_h denotes the energy gain or loss through elastic/inelastic reactions.

$$\text{Energy balance electrons : } \vec{\nabla} \cdot \left(\rho_e \varepsilon_e \vec{u} \right) + p_e \vec{\nabla} \cdot \vec{u} + \vec{\nabla} \cdot \vec{q}_e = Q_{Ohm} + Q_e$$

Q_{Ohm} is the energy gain through Ohmic heating.

$$Q_{Ohm} = \sigma E^2$$

Equation of state : $p = \sum_{\alpha} n_{\alpha} k_B T_{\alpha}$

The (axial) electric field is computed from the electric conductivity integrated over the cross section of the channel as:

$$I = \int_0^a 2\pi r \sigma(r) dr$$

Boundary conditions

Q.	Inlet	Outlet	Axis	Channel wall
p	$\frac{\partial p}{\partial z} = C$	$\frac{\partial p}{\partial z} = C$	$\frac{\partial p}{\partial r} = 0$	$\frac{\partial p}{\partial r} = 0$
u_z	$u_z = u_{in}^{max} \left[1 - \left(\frac{r}{R_{in}} \right)^2 \right]$	$u_z = u_{out}^{max} \left[1 - \left(\frac{r}{R_{in}} \right)^5 \right]$	$\frac{\partial u_z}{\partial r} = 0$	$u_z = 0$
u_r	$u_r = 0$	$\frac{\partial u_r}{\partial z} = 0$	$u_r = 0$	$u_r = 0$
$T_{e,h}$	$T_h = 500K$ $T_e = 6000K$	$\frac{\partial T_{e,h}}{\partial z} = 0$	$\frac{\partial T_{e,h}}{\partial r} = 0$	$T_h = 500^*K$ $T_e = 6000K / \frac{\partial T_e}{\partial r} = C$

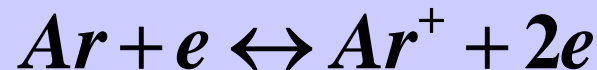
Chemical reactions inside arc channel

For reactions which are temperature dependent, Arrhenius like fit is used

$$k = c(T)^\beta \exp\left(\frac{-E}{T}\right)$$

Where c is the rate constant, T is the electron or heavy particle temp in eV, E is the reaction energy in eV and β is the power of Temp.

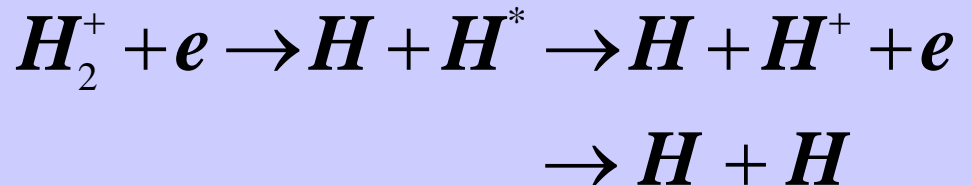
Argon ionisation:



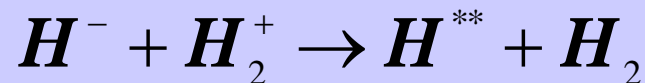
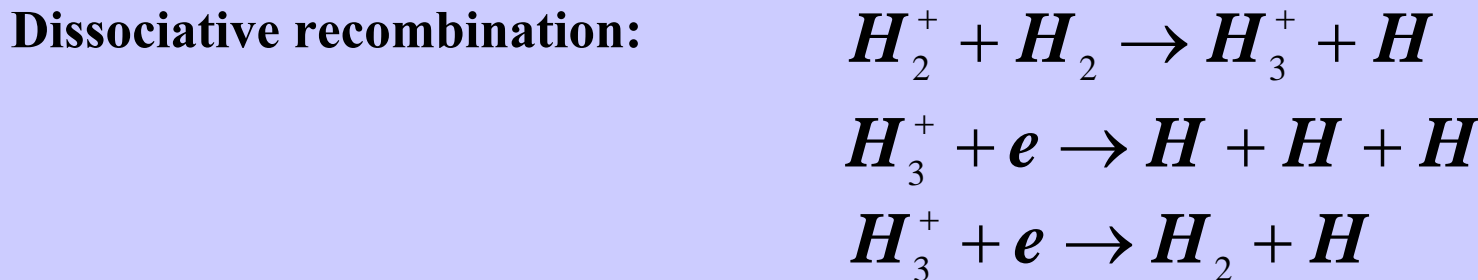
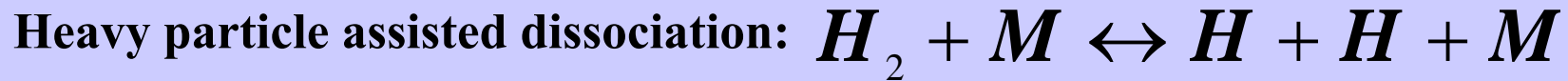
Molecular ionisation:



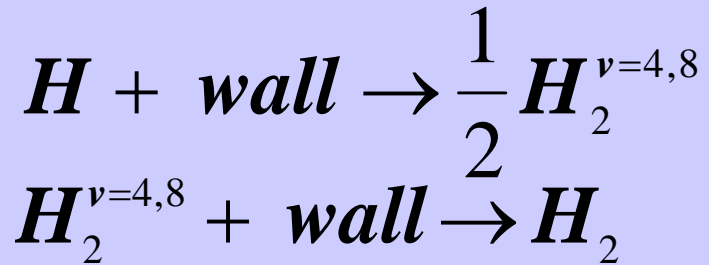
Dissociative recombination:



Dissociation by electron impact: $H_2^+ + e \rightarrow H + H^+ + e$

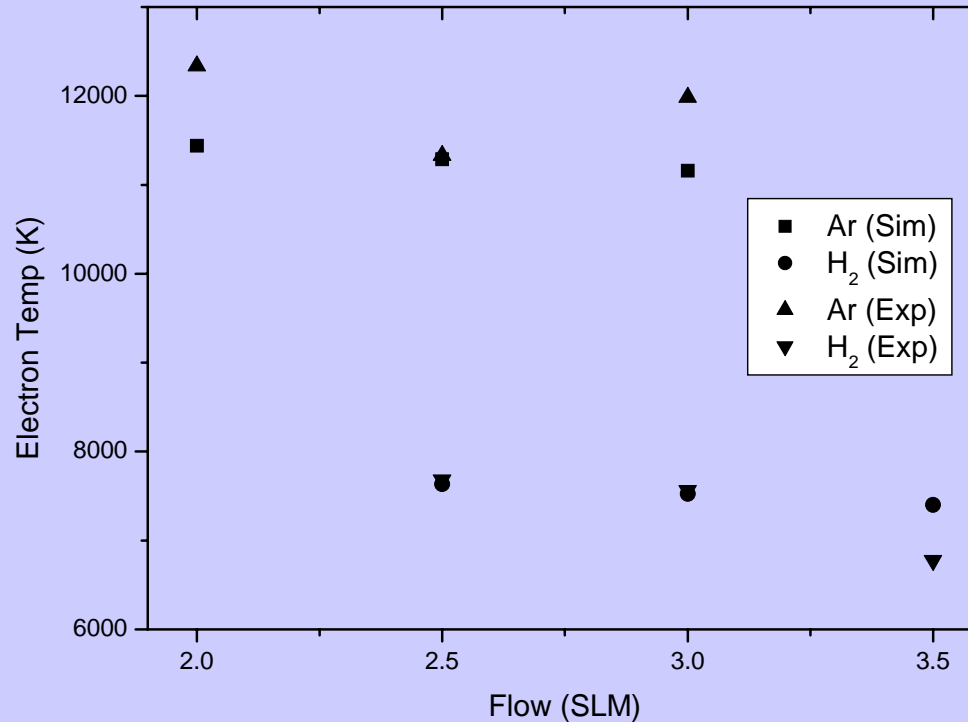


Chemical reactions at the channel walls

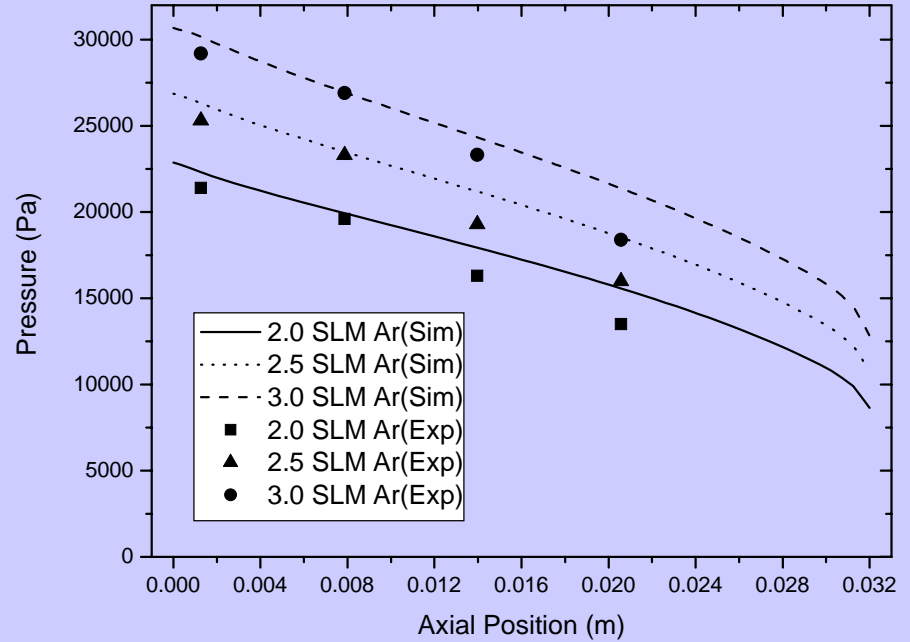
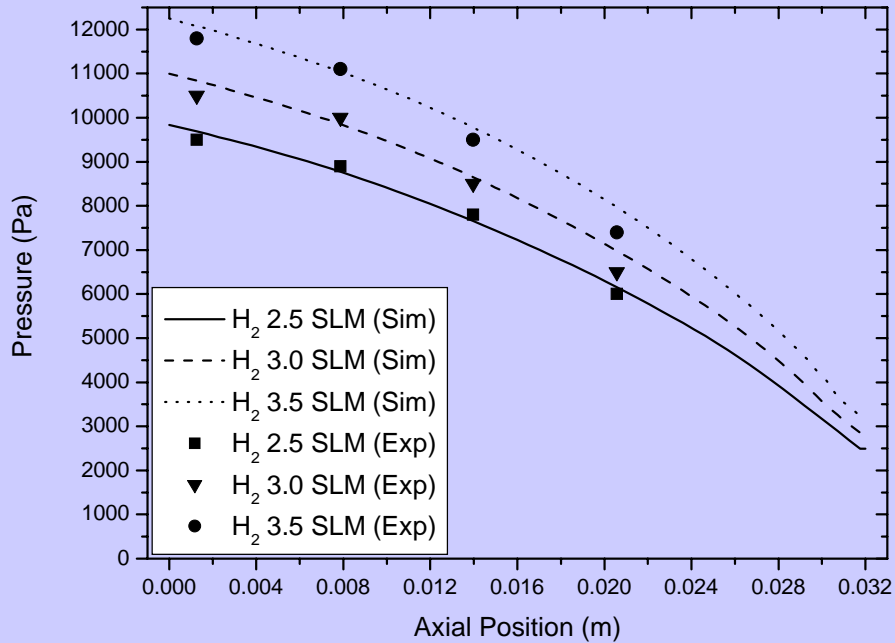


Results

Code to experiment validation for Pilot-psi

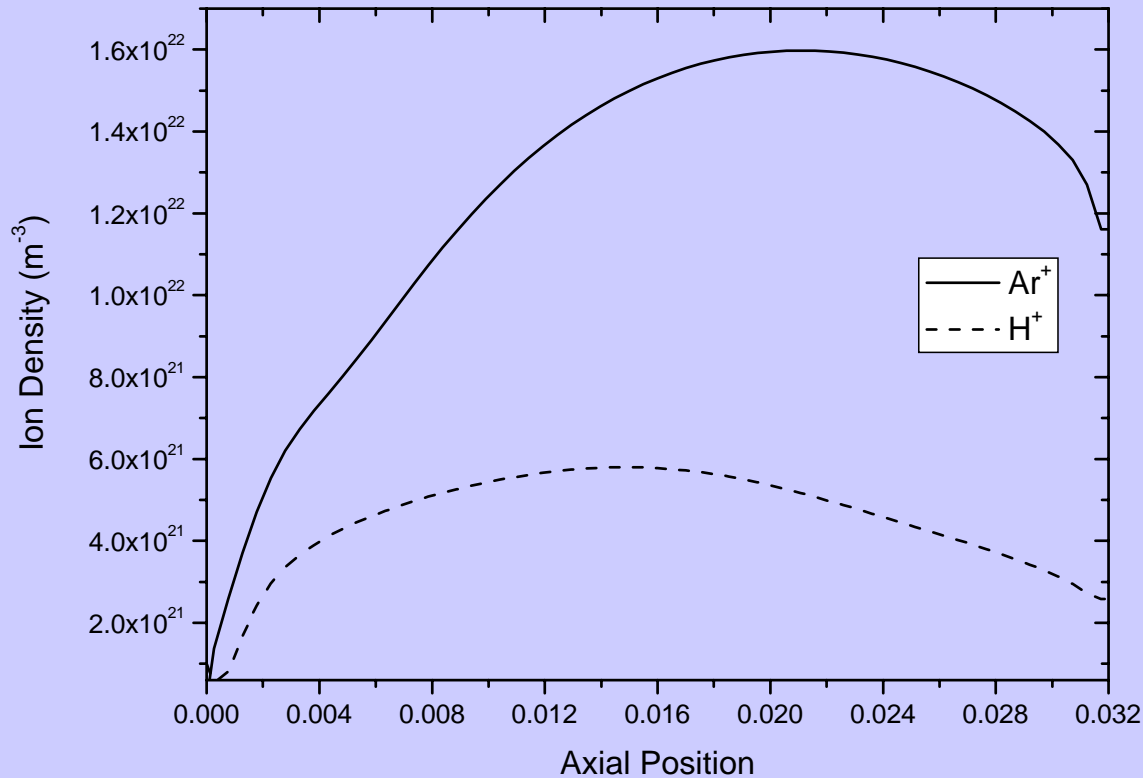


Comparison of temperature for Current 60 A, Flow 2.0, 2.5,3.0 SLM of Ar and 2.5, 3.0, 3.5 SLM of H₂



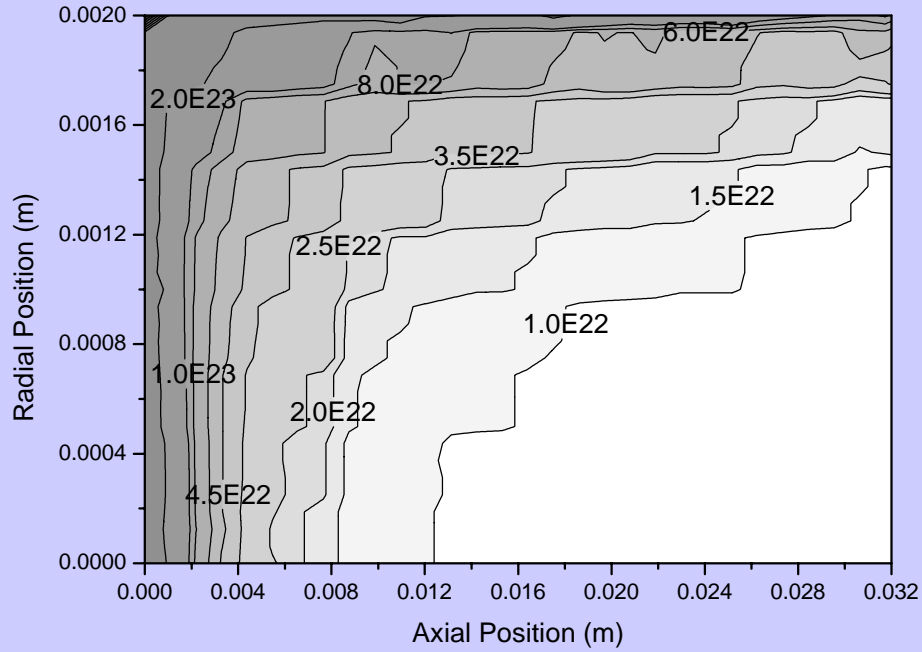
Comparison of experimental results for the pressure along the arc length

Ar⁺ and H⁺ densities along the axes with a 2mm radius operated at current of 60A and a flow of 2.5 and 3.0 SLM respectively

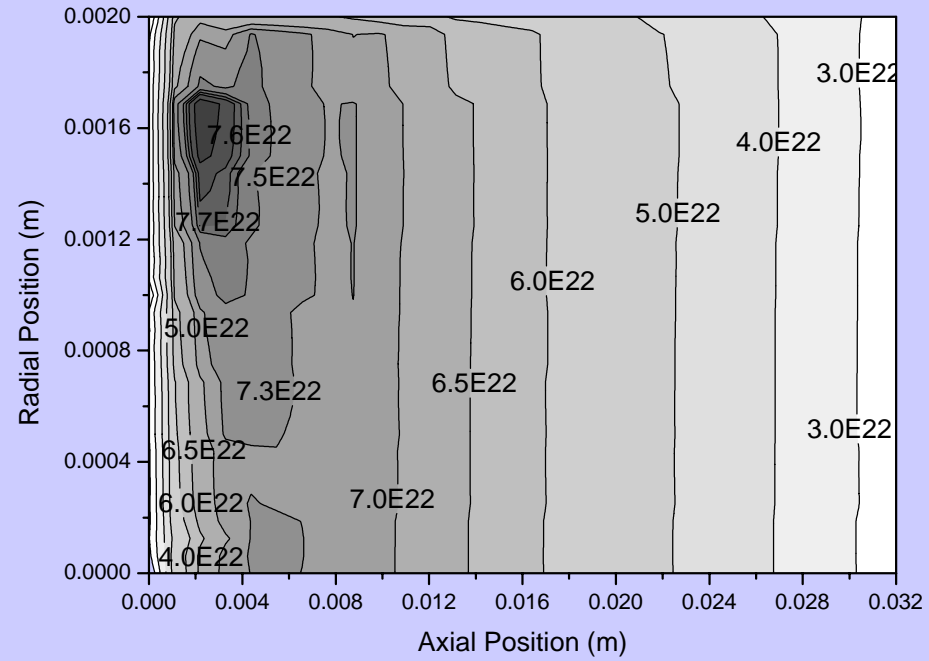


Profiles

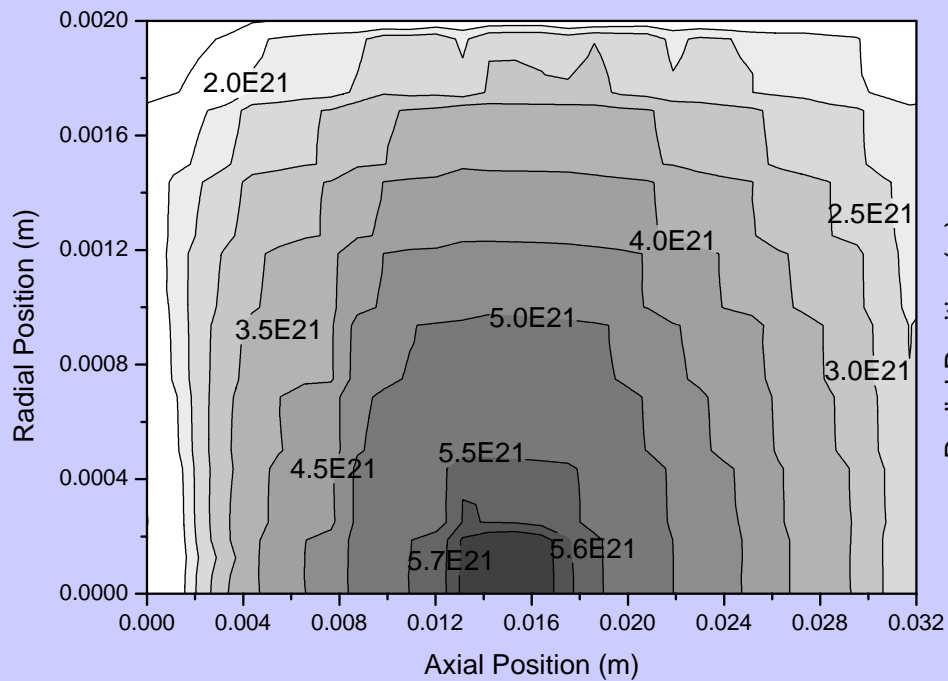
Current 60A, Flow 3.0 SLM



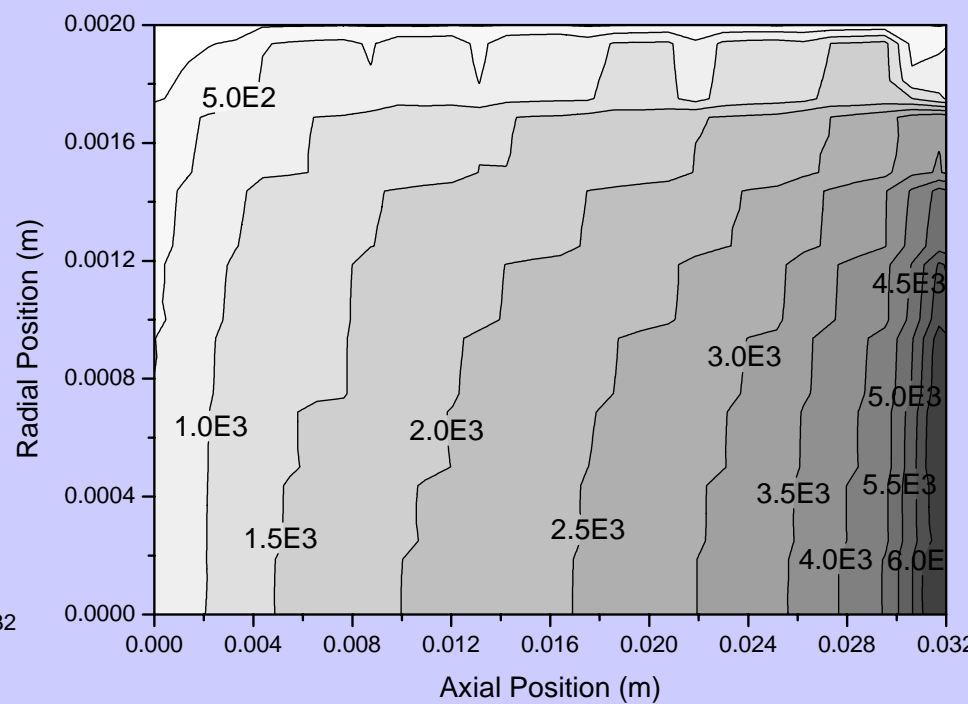
H_2



H



H^+



Velocity

Ion Fluxes and energy required for per ion for different geometries

Current (A)	R (mm)	L (mm)	H ⁺ flux (s ⁻¹)	H ⁺ (eV/ion)	Ionization %	Ar ⁺ flux (s ⁻¹)	Ar ⁺ (eV/ion)	Ionization %
60	2	30	1.38x10 ²⁰	320	5.4	1.58x10 ²⁰	87	14.5
60	2	32	1.39x10 ²⁰	343	5.4	1.64x10 ²⁰	91	15.1
60	2	40	1.44x10 ²⁰	427	5.6	1.87x10 ²⁰	98	17.1
410	5	30	1.39x10 ²¹	199	38	4.08x10 ²⁰	218	37.5
410	5	32	1.46x10 ²¹	201	37.6	4.37x10 ²⁰	216	40.1
410	5	70	2.15x10 ²¹	294	18.4	8.51x10 ²⁰	212	78.0

Magnetic Field Effect

Thermal Conductivity of electrons in the presence of ions and neutrals:

$$\kappa_e(0) = \frac{2.4}{\left(1.0 + \left(\frac{\nu_{ei}}{\sqrt{2}\nu_{e0}}\right)\right)} \frac{k_B^2 n_e T_e}{m_e \nu_{e0}}$$

In the presence of Magnetic field it is modified as:

$$\kappa_e(\mathbf{B}_{ext}) = \frac{1}{\left(1.0 + \left(\frac{\omega_{ce}}{\nu_{e0} + \nu_{ei}}\right)^2\right)} \kappa_e(0)$$

Where

$$\omega_{ce} = \frac{e\mathbf{B}_{ext}}{m_e}$$

The Ambipolar Diffusion coefficient

$$D_a = \frac{\mu_i D_e + \mu_e D_i}{\mu_i + \mu_e}$$

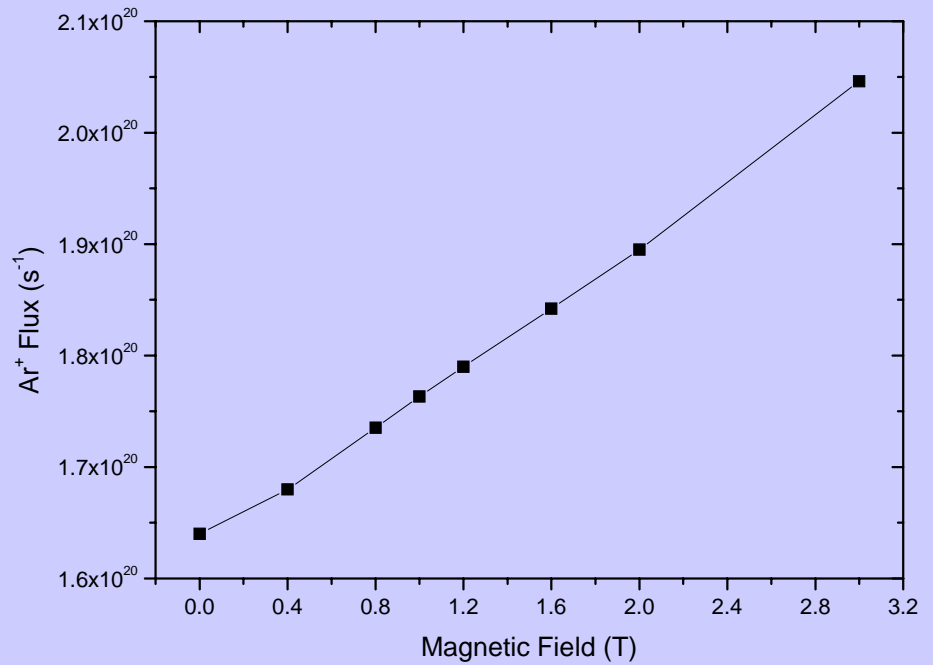
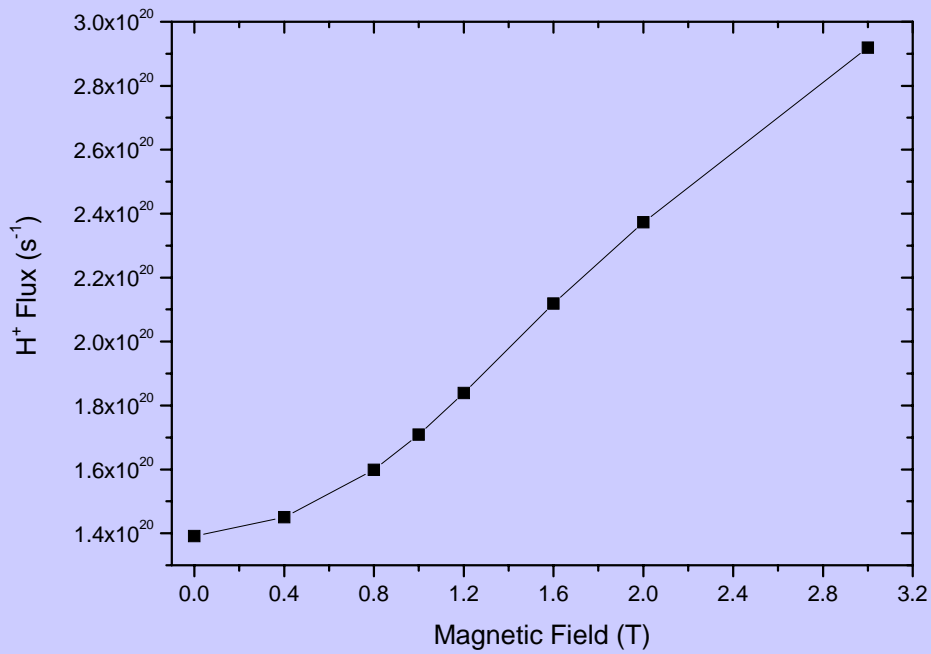
$$\mu_i = \frac{q}{m_i (v_{i0} + v_{ii} + v_{ie})}$$

$$\mu_e = \frac{q}{m_e (v_{e0} + v_{ei})}$$

In the presence of magnetic field, the electron transport coefficient are strongly reduced, and, in the limit where ion transport is dominant, the ambipolar diffusion coefficient becomes,

$$D_a = D_i \left(1 + \frac{T_e}{T_i} \right) \left(\frac{1}{1 + \frac{\mu_i}{\mu_e} \left(1 + \left(\frac{\omega_{ce}}{v_{e0} + v_{ei}} \right)^2 \right)} \right)$$

Fluxes leaving the Arc, Current 60A, Flow 3.0 SLM



Summary

- **It can be seen that simulation results are in reasonable agreement with the experimental findings.**
- **For the case of hydrogen arc lengthening the arc will not increase the ionization degree, however, widening the arc will increase the ionization degree which can be considered as a plasma source for Magnum-psi**
- **For the argon arc lengthening and widening the arc both increase the ionization degree.**
- **Both argon and hydrogen fluxes increase with the magnetic field. The Ar^+ flux is not much influenced by the magnetic field, only 25% at a field of 3T. The H^+ flux increases significantly, with a 3T magnetic field the flux is doubled.**

Thank you very much for your attention